# Solution to the Final Exam for ME218a Fall 1995 

## Problem 1.1



## Problem 1.2

At $3 \mathrm{~mW} / \mathrm{cm}^{2}$, the voltage is $5 \mathrm{~V}-\left(3 \mathrm{~mA}^{*} 1 \mathrm{~K}\right)=2 \mathrm{~V}$
At $2 \mathrm{~mW} / \mathrm{cm}^{2}$, the voltage is $5 \mathrm{~V}-(2 \mathrm{~mA} * 1 \mathrm{~K})=3 \mathrm{~V}$
So, as the light level drops the voltage rises by 1 V

## Problem 1.3

The sensor response is linear from approximately 0 to $5 \mathrm{~mW} / \mathrm{cm}^{2}$.
This corresponds to an output voltage range from $5 \mathrm{~V}-0 \mathrm{~V}$ in the circuit.
With a 10 V supply, the LM324 can easily get it's output up to 5 V .
On the lower range, the $\mathrm{V}_{\mathrm{ol}}$ is listed as 50 mV , max. corresponding to a light level of $4.95 \mathrm{~mW} / \mathrm{cm}^{2}$, so we would expect the output to be linear over the range of $0-4.95 \mathrm{~mW} / \mathrm{cm}^{2}$.

## Problem 1.4



The desired switch point is $3 \mathrm{~mW} / \mathrm{cm} 2$
This corresponds to a voltage of $5-3=2 \mathrm{~V}$
in order to get $+-0.03 \mathrm{mw} / \mathrm{cm} 2$ of hysterisis, set the switch points to
$\mathrm{V}_{\mathrm{a} 1}=2.03 \mathrm{~V}, \mathrm{~V}_{\mathrm{a} 2}=1.97 \mathrm{~V}$
choose Rpullup $=3.3 \mathrm{k}$
choose R3 = 1M, since we don't want a lot of hysterisis then, using the method of AN74

$$
\begin{gathered}
n=\frac{\Delta V_{a}}{V_{a 2}}=.030456 \\
\mathrm{R} 1=\mathrm{nR} 3=30456 \mathrm{~W} \\
R_{2}=\frac{R_{\|} \| R_{3}}{\frac{V_{c c}}{V_{a 1}}-1}=7528 \Omega
\end{gathered}
$$

If we go back and use the closest available value for R1 and use it to calculate R2, we come up with $33 \mathrm{~K} \Omega$ for R1 and $8.2 \mathrm{~K} \Omega$ for R 2 , which yields switch points of $2.04 \mathrm{~V} \& 1.98 \mathrm{~V}$.
For light levels below the threshold, the input would be high, forcing the output low.
For light levels above the threshold, the input would be low, forcing the output high (10V)

## Problem 1.5

From 68HC11
To LMD18200


| Mode is $====>$ | Coast | Brake | Run | Brake |
| :--- | :--- | :--- | :--- | :--- |
| Enable | 0 | 0 | 1 | 1 |
| Brake | 0 | 1 | 0 | 1 |
| PWM $=$ | 0 | 1 | 1 | 0 |

Relationship is Enable XOR Brake

| Mode is $====>$ | Coast | Brake | Run | Brake |
| :--- | :--- | :--- | :--- | :--- |
| Enable | 0 | 0 | 1 | 1 |
| Brake | 0 | 1 | 0 | 1 |
| BRAKE $=$ | 1 | 1 | 0 | 0 |

Relationship is NOT Enable
To get the motor leads connected to power when both PWM \& BRAKE are high requires that DIR also be high, so OR Direction with BRAKE to insure the if braking, DIR will be high.

## Problem 1.6

```
HEX
0000 CONSTANT TIMER
B004 CONSTANT PORTB
01 CONSTANT ENABLE_HI
FE CONSTANT ENABLE_LO
80 CONSTANT DIR_CW
7F CONSTANT DIR_CCW
20 CONSTANT BRAKE_HI
DF CONSTANT BRAKE_LO
2SECONDS CONSTANT 1E8 ( 488 TICKS = 2 SEC )
HALF_SECOND CONSTANT 7A ( }122\mathrm{ TICKS = 0.5 SEC )
: DELAY ( TICKS - )
    TIMER @
    + ( ADD NUMBER OF TICKS TO DELAY )
    BEGIN
            DUP
            TIMER @
            =
        UNTIL ( WAIT TILL TIMER = NEW VALUE )
    DROP
;
```

```
: DELAY2SECONDS ( - )
    2SECONDS
    DELAY
;
: DELAY_HALF_SECOND ( - )
    HALF_SECOND
    DELAY
;
: Coast ( - )
    PORTB C@
    ENABLE_LO AND
    BRAKE_LO AND
    PORTB C!
;
: Forward ( - )
        PORTB C@
        ENABLE_HI OR
        BRAKE_LO AND
        DIR_CW OR
        PORTB C!
        DELAY2SECONDS
        Coast
;
: Reverse ( - )
        PORTB C@
        ENABLE_HI OR
        BRAKE_LO AND
        DIR_CCW AND
        PORTB C!
        DELAY2SECONDS
        Coast
;
: Brake ( - )
        PORTB C@
        BRAKE_HI OR
        PORTB C!
        DELAY_HALF_SECOND
        Coast
```

    Problem 2.1
    (200
    

The switch points are at $3.496 \mathrm{~V} \& 3.835 \mathrm{~V}$

## Problem 2.2



## Problem 3.1



What's wrong?

1) It is configured for negative, not positive feedback.
2) there is no pull-up, the 339 has an open collector output.
3) The upper set-point exceeds the common mode voltage range.

To fix it, make it something like:


## Problem 3.2

What's wrong?
The voltage required at the base of the TIP110 is $1.5+\left(30 \mathrm{~mA}^{*} 80 \mathrm{~W}\right)+1.25 \mathrm{~V}=5.15 \mathrm{~V}$
This can never be achieved by the 74LS14, so the TIP110 will remain off, even though it will supply a legal high to the downstream gates.

To fix it, re-configure it like:


The $4.7 \mathrm{k} \Omega$ resistor was sized by noting that the voltage required at the base of the TIP110 is 1.25 V , while the minimum output voltage supplied by the LS14 is 2.7 V , so 1.45 V must be dropped across the resistor, while passing $0.3 \mathrm{~mA}(30 \mathrm{~mA} / 100)$. This indicates the need for a $4.83 \mathrm{k} \Omega$ resistor, $4.7 \mathrm{k} \Omega$ is the closest size that will deliver the required current. This will result in $1.45 / 47 \mathrm{k} \Omega=309 \mathrm{~mA}$ flowing. The 'LS14 is capable of sourcing 400 mA , while maintaining an output voltage of 2.7 V . The 4 LS inputs to be driven will require a total of $80 \mathrm{~mA}(4 * 20 \mathrm{~mA})$, so the total required output current is 389 mA , well within the 400 mA the 'LS14 is guaranteed to deliver.
The $91 \Omega$ resistor was sized by noting that the voltage at the top of the LED needs to be $2.2 \mathrm{~V}(0.7 \mathrm{~V}+$ 1.5 V ) when 30 mA is passing through the LED. this sets the $\Delta \mathrm{V}$ across the resistor, and the current is determined by the required 30 mA to the LED. This indicates the need for a $93.3 \Omega$ resistor. $91 \Omega$ is the closest standard size that will provide at least 30 mA , in fact it will provide 30.8 mA ,

## Problem 3.3

What's wrong?

1) The semicolon at the end of the for statement will insure that nothing gets executed by the for loop. 2) the comparisons to $\mathrm{A}, \mathrm{B} \& \mathrm{C}$ use the assignment operator ' $=$ ', not the comparison operator ' $==$ '.

To fix it:

1) remove the trailing semi-colon
2) correct the comparison operators.
